

The following formulas cover the basic calculations used in brake application engineering.

| Required   | Given   | Formula   |
|--|---|---|
| Full load motor torque ( $T_{flmt}$ ), lb-ft   | Horsepower (P), hp<br>Shaft speed (N), rpm<br>5252 = Constant   | $T_{flmt} = \frac{5252 \times P}{N}$                          |
| Average dynamic braking torque ( $T_d$ ), lb-ft  | Total inertia reflected to brake ( $Wk^2$ ), lb-ft <sup>2</sup><br>Shaft speed at brake (N), rpm<br>Desired stopping time (t), seconds<br>308 = Constant  | $T_d = \frac{Wk^2 \times N}{308 \times t}$                    |
| Static torque (T), lb-ft   | Force (F), lb<br>Pulley or drum radius, (R), ft   | $T = F \times R$  |
| Overhauling dynamic torque reflected to brake shaft ( $T_o$ ), lb-ft                               | Weight of overhauling load (W), lb<br>Linear velocity of descending load (V), ft/min<br>Shaft speed at brake (N), rpm<br>0.158 = Constant   | $T_o = \frac{0.158 \times W \times V}{N}$                     |
| Static torque of brake ( $T_s$ ), lb-ft<br>(General Guideline)                                     | Dynamic braking torque required ( $T_d$ ), lb-ft<br>0.8 = Constant (derating factor)  | $T_s = \frac{T_d}{0.8}$                                       |
| Inertia of rotating load reflected to brake shaft ( $Wk_b^2$ ), lb-ft <sup>2</sup>                 | Inertia of rotating load ( $Wk_L^2$ ), lb-ft <sup>2</sup><br>Shaft speed at load ( $N_L$ ), rpm<br>Shaft speed at brake ( $N_B$ ), rpm  | Equivalent $Wk_b^2 = Wk_L^2 \left( \frac{N_L}{N_B} \right)^2$ |
| Equivalent inertia of linear moving load reflected to brake shaft ( $Wk_w^2$ ), lb-ft <sup>2</sup> | Weight of linear moving load (W), lb<br>Linear velocity of load (V), ft/min<br>Shaft speed at brake ( $N_B$ ), rpm<br>$2\pi$ = Constant   | Equivalent $Wk_w^2 = W \left( \frac{V}{2\pi N_B} \right)^2$   |
| Kinetic energy of rotating load, ( $KE_r$ ), ft-lb   | Inertia of rotating load reflected to brake shaft ( $Wk_b^2$ ), lb-ft <sup>2</sup><br>Shaft speed at brake ( $N_B$ ), rpm<br>5875 = Constant  | $KE_r = \frac{Wk_b^2 \times N_B^2}{5875}$                     |
| Kinetic energy of linear moving load ( $KE_l$ ), ft-lb   | Weight of load (W), lb<br>Linear velocity of load (v), ft/sec<br>g = Gravitational acceleration constant, 32.2 ft/sec <sup>2</sup>  | $KE_l = \frac{Wv^2}{2g}$                                      |
| Change in potential energy (PE), ft-lb   | Weight of overhauling load (W), lb<br>Distance load travels (s), ft   | $PE = Ws$   |
| Total energy absorbed by brake ( $E_T$ ), ft-lb  | Total linear kinetic energy, ( $KE_L$ ), ft-lb<br>Total rotary kinetic energy ( $KE_R$ ), ft-lb<br>Potential energy converted to kinetic energy (PE), ft-lb   | $E_T = KE_L + KE_R + PE$                                      |
| Thermal capacity required for rotational or linear moving loads (TC), hp-sec/min                   | Total system inertia reflected to brake shaft ( $Wk_T^2$ ), lb-ft <sup>2</sup><br>Shaft speed at brake ( $N_B$ ), rpm<br>Number of stops per minute (n), not less than one $3.2 \times 10^6$ = Constant | $TC = \frac{Wk_T^2 \times N_B^2 \times n}{3.2 \times 10^6}$   |
| Thermal capacity required for overhauling loads (TC), hp-sec/min                                   | Total energy brake absorbs ( $E_T$ ), ft-lb<br>Number of stops per minute (n), not less than one 550 = Constant   | $TC = \frac{E_T \times n}{550}$                               |
| Linear velocity, ft/min  | N = rpm<br>Diameter (D), ft   | $V = N\pi D$  |